Modified Level II Streambed-Scour Analysis for Structure I-74-4-4415DRA Crossing Spring Creek in Vermillion County, Indiana

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Prepared in cooperation with the INDIANA DEPARTMENT OF TRANSPORTATION

U.S. GEOLOGICAL SURVEY Open-File Report 97-333



Indianapolis, Indiana 1997

U.S. DEPARTMENT OF THE INTERIOR BRUCE BABBITT, Secretary

U.S. GEOLOGICAL SURVEY Gordon P. Eaton, Director

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CONVERSION FACTORS AND ABBREVIATIONS

Multiply	Ву	To obtain
inch (in.)	25.4	millimeter
foot (ft)	0.3048	meter
square foot (ft²)	929.0	square centimeter
feet per second (ft/s)	0.3048	meters per second
cubic foot per second (ft ³ /s)	0.02832	cubic meter per second
mile (mi)	1.609	kilometer
square mile (mi ²)	2.590	square kilometer

Abbreviations used in this report:

D_{50}	median diameter of bed material
Q100	100-year discharge
FEMA	Federal Emergency Management Agency
HEC	Hydraulic Engineering Circular
IDNR	Indiana Department of Natural Resources
INDOT	Indiana Department of Transportation
USGS	U. S. Geological Survey
WSPRO	Water Surface PROfile model

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ABSTRACT

Level II scour evaluations follow a process in which hydrologic, hydraulic, and sediment-transport data are evaluated to calculate the depth of scour that may result when a given discharge is routed through a bridge opening. The results of the modified Level II analysis for structure I-74-4-4415DRA, the southwest ramp crossing Spring Creek at the intersection of Interstate 74 and State Road 63 in Vermillion County, Indiana, are presented. The site is in northern Vermillion County near the town of Foster, which is in southern Warren County. Scour depths were computed with the Water Surface PROfile model, version V050196, which incorporates the scour-calculation procedures outlined in Hydraulic Engineering Circular No. 18. Total scour depths at the piers were approximately 8.8 feet for the modeled discharge of 4,500 cubic feet per second and approximately 9.8 feet for the modeled discharge of 6,600 cubic feet per second.

INTRODUCTION

The U.S. Geological Survey (USGS), in cooperation with the Indiana Department of Transportation (INDOT), is conducting Level II scour analyses at a number of bridges throughout Indiana. This report describes the methods applied and the modeling results for bridge I-74-4-4415DRA.

Background and Scope

Level I scour assessment is a process where a large number of bridges are studied as a group. Assessments usually are made by evaluating a combination of geomorphic, hydrologic, and bridge-characteristic data. The results help investigators determine which bridges appear to be most likely to experience streambed-scour problems and which bridges appear to be relatively immune to problems brought on by streambed scour (for example, bridges built on bedrock).

When applied correctly, Level I scour assessments provide an investigator with information to identify those bridges that appear to be relatively safe and those bridges that fall into higher risk categories.

Level II scour evaluations describe the process for an investigator to apply a model to a bridge site and calculate the potential depth of scour that may result from a given flood event. Level II analyses involve the application of basic hydrologic, hydraulic, and sediment-transport engineering concepts and may include an evaluation of flood history, channel hydraulic conditions (for example, water-surface profile analysis), and basic sediment-transport analyses such as scour calculations (Lagasse and others, 1995).

The methods and model outlined in Hydraulic Engineering Circular (HEC) No. 18 (Richardson and Davis, 1995) formulate the basis for Level II scour evaluations. Methods used in this study for Level II scour evaluations are a modification of the HEC-18 standards. These modifications were made to comply with the methodology requested by INDOT (Merril Dougherty, Indiana Department of Transportation, oral commun., 1996). Descriptions of the specific modifications are given in the "Evaluation Methods" section of this report.

This report presents the methods followed for modeling, special considerations for this study site, and the input for and the output from the Water Surface PROfile (WSPRO) model.

Site Description

The study site is located in northern Vermillion County near the town of Foster, which is just across the county line in southern Warren County. The drainage area for the site is approximately 22.6 mi² (Merril Dougherty, Indiana Department of Transportation, written commun., 1997). The predominant land use in the basin is rural; in the immediate vicinity of the bridge, the land is predominantly forest.

Within the immediate vicinity of the bridge, Spring Creek has a channel-bed slope of approximately 0.0026 ft/ft. The channel-bed material is gravel, and the channel banks consist of silt-clay. At the time of the Level I site visit on June 11, 1991, the banks were observed to have 10 to 90 percent woody vegetative cover; the field report noted that the banks were experiencing fluvial erosion.

The Interstate 74 ramp crossing of Spring Creek is a 112-ft-long, two-lane bridge consisting of three spans supported by concrete and steel piers and sloping riprap-covered spill-through abutments. Additional details describing conditions at the site are included in the Level I data base (Hopkins and Robinson, unpub. data, 1997). Photographs of the site, taken at the time of the Level I site visit, are archived at the USGS office in Indianapolis.

EVALUATION METHODS

The methods described in this section apply to a number of bridge sites in Indiana being evaluated for scour and outline the procedures requested by INDOT for these modified Level II scour analyses. The principal modification requested by INDOT was that the input data to the model come from or be estimated from existing data sources; no additional field data were collected. Actual methods used in the scour evaluation at this particular bridge site use the most applicable method possible, given the data available.

To determine drainage area, either published values found in Hoggatt (1975) or USGS 7.5-minute topographic maps with Hoggatt's original drainage-area delineations were used. Where there are no published data, drainage-area segments measured from the maps produced by Hoggatt were either subtracted from downstream sites or added to upstream sites published by Hoggatt (1975).

In Indiana, flood discharges are coordinated by agreement among State and Federal agencies. At sites where flood discharges officially are coordinated among State and Federal agencies in Indiana, the coordinated 100-year discharge (Q100) was modeled. INDOT also provided an additional flood discharge for these coordinated sites in excess of the Q100 to be modeled.

If a flood discharge was not coordinated, the USGS examined Federal Emergency Management Agency (FEMA) studies for Q100 determinations. Where FEMA studies did not produce a Q100, the USGS contacted IDNR for an estimated Q100 in the vicinity of the site being studied. If IDNR did not have a Q100, data from nearby USGS streamflow-gaging stations were analyzed with nearby and similar drainage basins that have been coordinated. At sites having no coordinated discharge data, the two discharges used in the model were 1) the approximated Q100 and 2) a discharge equal to 1.7 times the approximated Q100.

Most of the cross-section and bridge-opening geometry data were taken from the bridge plans (Indiana State Highway Commission, 1979) provided by INDOT. Bridge plans are presumed to be representative of current conditions at the site. To determine the cross-section geometry, a line was drawn on the bridge plans parallel to the bridge stationing and approximately one bridge width from the bridge. For sites where the bridge plans did not extend far enough laterally for collection of all cross-section data required for WSPRO model analysis, additional data were collected from 7.5-minute topographic maps.

The roadway and embankment profile was taken from the bridge and highway plans for those sites where roadway overtopping was expected. The INDOT bridge plans and 7.5-minute topographic maps were used as a guide, based on the water-surface elevations calculated by the WSPRO model, to determine if roadway overtopping might occur.

Roughness values (*n*-values) for the main channel were estimated by viewing photographs archived from the Level I scour assessments. The *n*-values for the overbanks were assigned on the basis of the surface-cover data summarized in the Level I data base (Hopkins and Robinson, unpub. data, 1997). From those data, the following roughness values were assigned to the surface-cover categories: urban—0.050, suburban—0.035, row crop—0.045, pasture—0.035, brush—0.120, forest—0.100, and wetland (any area covered by standing water)—0.100. The *n*-values for the overbanks were adjusted if the Level I photographs provided sufficient detail to warrant an adjustment.

WSPRO version V050196 was used to model flow through the study site. Starting watersurface elevation was obtained with a slope-conveyance computation. The channel-bed slope in the immediate vicinity of the bridge was estimated from the 7.5-minute topographic map and was used as the slope of the energy grade line for this computation.

WSPRO version V050196 includes a field that allows the input of up to four scour-adjustment factors (K1 to K4). For this modeling, the default value for K4 (bed armoring) was chosen. For scour-adjustment factors K1 and K2 (pier-nose shape and angle of attack, respectively), input values were determined by evaluating the data archived in the Level I data base (Hopkins and Robinson, unpub. data, 1997). For the K3 factor (bed forms), a value of 1.1 was applied in all cases.

In some cases, piers set on the overbanks are constructed with footings that are higher in elevation than pier footings in the main channel. In these situations, if the channel position changes, the piers that were initially constructed on the overbank may become part of the main channel. Therefore, to evaluate total potential scour, the model results obtained for contraction scour and deepest local scour in the main channel were added and applied to all piers in the bridge opening. This methodology allowed for an evaluation of potential undermining of pier supports in the event that future channel movement placed overbank piers in the main channel.

Where bridge pairs have a continuous abutment or fill between the bridges that does not allow expansion of flow, the bridge pair was modeled as one bridge. Sites with discontinuous abutments, allowing expansion between the bridges, were modeled as two separate bridges. In those cases, a valley cross section was measured between the bridges and used as the approach section for the downstream bridge and as the exit section for the upstream bridge.

At sites with no embankment to function as a weir or at sites where the tailwater drowns out the embankment, a composite bridge and road section was used to compute flow. Those sites were computed with friction-loss equations rather than with a bridge routine.

Total scour is taken as the sum of local scour plus contraction scour. If the model predicted negative contraction scour (aggradation), the contraction-scour value was assumed to be zero in determining the total scour depth (table 1). This assumption was made so that a negative contraction scour would not mask the potentially detrimental effects of local scour at a pier. No abutment scour evaluations were made in this study.

Table 1. Cumulative scour depths for the modeled discharges at structure I-74-4-4415DRA crossing Spring Creek in Vermillion County, Indiana

Pier number ¹	Stationing from bridge plans ²	Initial bed- elevation at pier (feet)	Main- channel contrac- tion scour depth (feet)	Local scour depth (feet)	Worst- case total- scour depth ³ (feet)	Bottom elevation of pier (feet)	Worst- case bed elevation after scour ⁴ (feet)
		Modeled	discharge ⁵ is 4,5	00 cubic feet p	per second		
1	11+78	544	0	8.8	8.8	536.0	534.0
2	12+22	544	0	8.8	8.8	536.0	534.0
		Modeled	discharge is 6,60	00 cubic feet p	er second		
1	11+78	544	0.1	9.7	9.8	536.0	533.0
2	12+22	544	0.1	9.7	9.8	536.0	533.0

¹Pier numbers were assigned from left to right as shown on the bridge plans.

²Stationing is the center line of the pier as determined from the bridge plans. Stationing from bridge plan, 11+78, represents a point 1,178 feet from an arbitrary starting location referenced on the bridge plans.

³Worst-case total-scour depths are generated by summing the calculated contraction-scour depth with the worst case of local scour.

⁴Worst-case bed elevation is computed by subtracting the worst-case total-scour depth from the lowest initial bed elevation in the bridge opening (542.8 feet).

⁵Not a coordinated discharge.

SPECIAL CONSIDERATIONS

Model runs indicate the water-surface elevation at the bridge is lower than the low-steel elevation for the modeled discharges. Therefore, there should be no pressure flow through the bridge opening for the discharges modeled.

Based on the bridge plans (Indiana State Highway Commission, 1979) and the field report from the Level I assessment, the piers appear to be protected by the riprap cover of the slopewall. The upstream side of pier 1 is protected by a concrete guidewall. The bridge was modeled and scour was computed as if these protective measures did not exist.

RESULTS

Scour depths were computed with a version of WSPRO (Larry Arneson, Federal Highway Administration, written commun., 1996) modified from Shearman (1990). This version of WSPRO includes scour calculations in the model output. Scour depths were calculated assuming an infinite depth of material that could erode and a homogeneous particle-size distribution. The results of the scour analysis are presented in table 1; a complete input file and output results are presented in the appendix.

REFERENCES

- Hoggatt, R.E., 1975, Drainage areas of Indiana streams: U.S. Geological Survey, Water Resources Division, 231 p.
- Indiana State Highway Commission, 1979, Bridge plans Interstate Route 74: Bridge File I-74-4-4415DRA.
- Lagasse, P.F.; Schall, J.D.; Johnson, F.; Richardson, E.V.; and Chang, F., 1995, Stream stability at highway structures (2d ed.): Federal Highway Administration, Hydraulic Engineering Circular No. 20, Publication FHWA-IP-90-014, 144 p.
- Richardson, E.V., and Davis, S.R., 1995, Evaluating scour at bridges (3d ed.): Federal Highway Administration, Hydraulic Engineering Circular No. 18, Publication FHWA-IP-90-017, 204 p.
- Shearman, J.O., 1990, User's manual for WSPRO, a computer model for water-surface profile computations: Federal Highway Administration Publication FHWA-IP-89-027, 177 p.

APPENDIX

WSPRO INPUT FILE

```
T1
         I-74 RAMP OVER SPRING CREEK I74-4-4415DRA
         COUNTY: VERMILLION
T2
                                    QUAD: PERRYSVILLE 93C
Т3
         7-30-97
                                    JOHN T. WILSON
Q
         4500
               6600
         .0026 .0026
SK
XS EXIT 0
         1043 570 1053 560 1145 550 1159 542.8 1190 542.8 1204 550
GR
GR
         1310 560
N
         .100
                .040 .100
           1145 1204
SA
XS
   FULLV 126
BR BRDGE 126 560.0
                     20
         ***BRIDGE DECK IS SKEWED 20 DEGREES (FROM BRIDGE PLANS) ***
         ***BASE OF PIERS ARE SET IN RIPRAP SLOPEWALLS***
         ***PIER 1 IS PROTECTED BY CONCRETE GUIDE WALL***
GR
         1138 560.0 1182 542.8 1219 542.8
        1264 561.5 1138 560.0
GR
N
        .038
PD
        544.0
              1.5
                     2
PD
        544.0 1.5
        544.4
               3.0
                     3
PD
        3 40 2
                     558
CD
DC 0 BRDGE 1153 1247 1206
                            1265 * 3
         ***DC LIMITS AT BRIDGE ARE APPROX. LEW AND REW FOR Q1***
                         PW * * K1 K2 K3
         BXL
              BXR
                1264.0
         1138.0
                         1.5 * * 1
                                      2.0 1.1
DP
         1138.0 1264.0 1.5 * * 1
                                      2.0 1.1
DP
         ***DP CARDS USE THE WHOLE BRIDGE OPENING FOR BXL/BXR***
*
XS APPR 292
        1137 570 1151 560 1206 550 1219 542.8 1251 542.8 1265 550
GR
        1394 550 1458 565
GR
         .100 .040 .100
N
            1206
                     1265
HP 2 BRDGE 554.4 * 554.4 4500
HP 2 BRDGE 556.4 * 556.4 6600
EΧ
ER
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Feder Run	Date & Time: put File: spri	ainistration ater-Surface 8/ 6/97 11:	- U.S.Geo Profile Compo 29 am Veo utput File:	ological Surve utations. rsion V050196 spring.LST	
	I-74 RAMP OVER				
	COUNTY: VERMII			RRYSVILLE 930	2
	7-30-97		JOHN T.		
Q	4500 6600				
*** Proc	essing Flow Da	ta; Placing	Information :	into Sequence	1 ***
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		inistration ter-Surface	- U.S.Geo	ological Surve	
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	310 560				
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1159.000	542.800	1190.000	542.800	1204.000	550.000
1310.000	560.000		512.000	1201.000	550.000

Maximum X-1 Minimum Y-1	Station: 1 Station: 1 Elevation: Elevation: Rough	542.800 (as 570.000 (as ness Data (ssociated Y-1 ssociated Y-1 ssociated X-3 ssociated X-3	Elevation: 5 Elevation: 5 Station: 11 Station: 10	60.000) 90.000)
		Roughness Coefficient			
			-	-	
	1	.100			
	2		1145.000		
	2	.040	1204.000		
	3	.100			
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	Finished				
	rinished	-			
*COUN	Highway Adm Model for Wa Input Units: I-74 RAMP OV Y: VERMILLIO	ter-Surface I English / C ER SPRING CRI	Profile Compu Output Units: CEK 174-4-4	tations. English 1415DRA SVILLE 93C	
•	7-30-97		JOHN T.	MITPON	
*	Starting '	To Process He	eader Record	FULLV *	
+++ Comm1.	tod Donding 1	Data Aggogiat	od With Hood	low Dogowd Ell	T.T.V ***
*** No Rou	eted Reading Data : g X-Section Data	Input, Propag	gating From I	Previous Sect	ion ***
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Х	Y	X	Y	x	Y
1042 000	570.000	1053 000	560 000	1145 000	550 000
1043.000 1159.000	542.800	1053.000 1190.000	560.000 542.800		550.000 550.000
1310.000	560.000				

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Minimum and Maximum X, Y-coordinates
 Minimum X-Station:
                   1043.000 (associated Y-Elevation: 570.000)
 Maximum X-Station:
                   1310.000 (associated Y-Elevation: 560.000)
 Minimum Y-Elevation: 542.800 (associated X-Station: 1190.000)
 Maximum Y-Elevation:
                    570.000 (associated X-Station:
                                               1043.000 )
                Roughness Data ( 3 SubAreas )
                      Roughness
                               Horizontal
              SubArea Coefficient Breakpoint
                     -----
                        .100
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                                1145.000
                        .040
                        - - -
                               1204.000
                3
                        .100
                     *-----
            Finished Processing Header Record FULLV
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  ******************* W S P R O ***************
    Federal Highway Administration - U. S. Geological Survey
          Model for Water-Surface Profile Computations.
         Input Units: English / Output Units: English
  *----*
          I-74 RAMP OVER SPRING CREEK I74-4-4415DRA
      COUNTY: VERMILLION
                              OUAD: PERRYSVILLE 93C
         7-30-97
                                 JOHN T. WILSON
       *-----*
            Starting To Process Header Record BRDGE
       *-----
BR
   BRDGE 126 560.0 20
GR
       1138 560.0 1182 542.8 1219 542.8
        1264 561.5 1138 560.0
GR
N
       .038
       544.0
              1.5
PD
                    1
PD
       544.0
              1.5
                    2
PD
       544.4
              3.0
                    3
CD
       3 40 2
                    558
***
     Completed Reading Data Associated With Header Record BRDGE
***
     Storing Bridge Data In Temporary File As Record Number 3
                                                      ***
***
              Data Summary For Bridge Record BRDGE
SRD Location:
               126. Cross-Section Skew: 20.0
                                           Error Code
Valley Slope: ******
                     Averaging Conveyance By Geometric Mean.
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Energy Loss Coefficients -> Expansion: .50 Contraction: .00

Х	X,Y Y	-coordinates X	(5 pairs) Y	x	Y
1138.000	560.000	1182.000	542.800 560.000		542.800
Maximum X- Minimum Y- Maximum Y- X-coor	Station: Station: Elevation: Elevation: dinates & Ho	and Maximum 1138.000 (a 1264.000 (a 542.800 (a 561.500 (a	associated Y- associated Y- associated X- associated X- akpoints Tran	Elevation: 5 Elevation: 5 Station: 12 Station: 12 slated by Ske	561.500) 219.000) 264.000)
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		1182.000 1138.000		1219.000	1219.000
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******************* W S P R O ***************
    Federal Highway Administration - U. S. Geological Survey
          Model for Water-Surface Profile Computations.
         Input Units: English / Output Units: English
  *-----
          I-74 RAMP OVER SPRING CREEK I74-4-4415DRA
      COUNTY: VERMILLION QUAD: PERRYSVILLE 93C
         7-30-97
                                 JOHN T. WILSON
DC 0 BRDGE 1153 1247 1206 1265 * 3
        1138.0 1264.0 1.5 * * 1 2.0 1.1
DP
        1138.0 1264.0 1.5 * * 1 2.0 1.1
       *-----
            Starting To Process Header Record APPR
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   APPR 292
       1137 570 1151 560 1206 550 1219 542.8 1251 542.8 1265 550
GR
        1394 550 1458 565
N
       .100 .040 .100
            1206 1265
SA
***
    Completed Reading Data Associated With Header Record APPR
*** Storing X-Section Data In Temporary File As Record Number 4 ***
              Data Summary For Header Record APPR
                                                      ***
               292. Cross-Section Skew: .0 Error Code 0
SRD Location:
Valley Slope: .00000 Averaging Conveyance By Geometric Mean.
Energy Loss Coefficients -> Expansion: .50 Contraction: .00
                X,Y-coordinates (8 pairs)
                 X Y
   Х
                  570.000
                                        1206.000
                     1151.000
                               560.000
 1137.000
                                                    550.000
 1219.000
          542.800
                    1251.000
                              542.800
                                        1265.000
                                                   550.000
 1394.000
          550.000
                   1458.000
                               565.000
                    -----
             Minimum and Maximum X, Y-coordinates
 Minimum X-Station: 1137.000 (associated Y-Elevation: 570.000)
 Maximum X-Station: 1458.000 (associated Y-Elevation: 565.000)
 Minimum Y-Elevation: 542.800 (associated X-Station: 1251.000)
 Maximum Y-Elevation: 570.000 (associated X-Station: 1137.000)
                Roughness Data ( 3 SubAreas )
                      Roughness Horizontal
              SubArea Coefficient Breakpoint
                    ....... ......
                        .100
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                        .040
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                                1265.000
                        .100
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SRD: .000	550.168		.613	*****	1.409	*****	
Section: FULLV Header Type: FV	554.112 554.975	.864 .303	4500.000 6.131	733.942 95533.58	126.000 126.000	1107.174 1247.583	
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<<< The Following Data Reflect The "Constricted" Profile >>>
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	WSEL EGEL CRWS	HF	v	AREA K SF	FLEN	
Section: BRDGE Header Type: BR SRD: 126.000	554.932	.266	5.991	113871.00	126.000	1246.606
Specific Bridge Bridge Type 3 Pier/Pile Code	Flow Type 1					
	WSEL	מחמ	0	AREA	CDDI	LEW
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Section: APPR Header Type: AS SRD: 292.000	EGEL CRWS 554.825 555.234 550.722	HF HO .410 .218 .079	V FR # 4500.000 3.337 .378	K SF 1348.319 132837.10 .0016	FLEN ALPHA 126.000 156.209 2.364	REW ERR 1179.464 1414.585
Header Type: AS SRD: 292.000 App M(G	EGEL CRWS 554.825 555.234 550.722 Froach Section	HF HO .410 .218 .079 on APPR KQ	V FR # 4500.000 3.337 .378 Flow Cont XLKQ	K SF 1348.319 132837.10 .0016 raction Info	FLEN ALPHA 126.000 156.209 2.364 rmation	REW ERR 1179.464 1414.585

<<< End of Bridge Hydraulics Computations >>>

Model for Water-Surface Profile Computations.

Input Units: English / Output Units: English

I-74 RAMP OVER SPRING CREEK I74-4-4415DRA

COUNTY: VERMILLION 7-30-97

QUAD: PERRYSVILLE 93C JOHN T. WILSON

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: EXIT Header Type: XS SRD: .000	555.777 556.986 552.024		6600.000 6.632 .649	995.248 129407.80 *****		1091.851 1265.237 *****
Section: FULLV Header Type: FV SRD: 126.000	556.197	1.090	6600.000	1069.781	126.000	1087.989
	557.287	.305	6.169	138960.20	126.000	1269.687
	552.024	.000	.608	.0024	1.842	004

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

===135 CONVEYANCE RATIO OUTSIDE OF RECOMMENDED LIMITS AT SECID "APPR ". KRATIO: 1.45

Section: AF	PR 557.082	.462	6600.000	1903.820	166.000	1167.052
Header Type	e: AS 557.544	.259	3.467	201253.90	166.000	1424.215
SRD: 292	.000 552.220	.000	.353	.0016	2.472	002

<<< The Preceding Data Reflect The "Unconstricted" Profile >>>

<<< The Following Data Reflect The "Constricted" Profile >>>
 <<< Beginning Bridge/Culvert Hydraulic Computations >>>

	WSEL	VHD	Q	AREA	SRDL	LEW
	EGEL	HF	V	K	FLEN	REW
	CRWS	HO	FR #	SF	ALPHA	ERR
Section: BRDGE	556.296	.968	6600.000	951.475	126.000	1147.475
Header Type: BR	557.264	.281	6.937	157513.50	126.000	1251.477
SRD: 126.000	551.251	.000	.460	*****	1.294	.014
Specific Bridge Bridge Type 3 Pier/Pile Code	Information Flow Type 1 0	C .8793		ELEV BLEN 0.000 ******	XLAB	XRAB * ******

	-	WSEL EGEL CRWS	НО	Q V FR #	AREA K SF	FLEN ALPHA	REW ERR
	n: APPR				1911.686		
	Type: AS						
SRD:	292.000	552.220	.080	.351	.0016	2.4/3	006
		M(K)	KQ	XLKQ	raction Inf XRKQ	OTEL	
	.59				53 1294.387		
**	<<< ******* Federal Hig	*****	** W S P	RO ***		*****	
	_	_			Computatio	_	
					Units: Engl		
*-		RAMP OVER	R SPRING C	REEK I	74-4-4415DR PERRYSVILLE HN T. WILSO	A 93C	*
***					Header Reco r Record Nu		***
	Water Surfac	e Elevatio	n: 554	400	_		
						lement # 1	
	Flow: 450	0.000 Ve	elocity:	5.90 ну	draulic Dep	th: 8.06	9
(Cross-Section	0.000 Ve n Area:	elocity: 763.22	5.90 Нус Сс	draulic Dep onveyance:	th: 8.06 116403.6	9
(Cross-Section	0.000 Ve n Area:	elocity: 763.22	5.90 Hyo Со	draulic Dep	th: 8.06 116403.6	9
	Cross-Section Bank Stat	0.000 Ven Area: ions -> I	elocity: 763.22 Left: 11	5.90 нус 52.326	draulic Dep onveyance: Right: 1	th: 8.06 116403.6 246.915	9 0 1186.5
X STA.	Cross-Section Bank Stat 1152.3	0.000 Ven Area: ions -> I 1171.0	elocity: 763.22 ueft: 11) 1176 45.8	5.90 Hyo Co 52.326 .5 13 40.7	draulic Deponveyance: Right: 1 180.5 1 7 35.	th: 8.06 116403.6 246.915 183.5 3 33	9 0 1186.5
X STA. A(I) V(I)	Cross-Section Bank Stat 1152.3	0.000 Ven Area: ions -> I 1171.0 68.3 3.30	elocity: 763.22 Left: 11) 1176 45.8 4.91	5.90 Hyo Co 52.326 .5 1: 40.7 5.53	draulic Deponveyance: Right: 1 180.5 1 7 35. 3 6.3	th: 8.06 116403.6 246.915 183.5 3 33 8 6.	9 0 1186.5 .9 63
X STA.	Cross-Section Bank Stat 1152.3	0.000 Ven Area: ions -> I 1171.0 68.3 3.30	elocity: 763.22 Left: 11) 1176 45.8 4.91	5.90 Hyo Co 52.326 .5 1: 40.7 5.53	draulic Deponveyance: Right: 1 180.5 1 7 35.	th: 8.06 116403.6 246.915 183.5 3 33 8 6.	9 0 1186.5 .9 63
X STA. A(I) V(I) D(I)	Cross-Section Bank Stat 1152.3	0.000 Ven Area: ions -> I 1171.0 68.3 3.30 3.65	elocity: 763.22 Left: 11 0 1176 45.8 4.91 8.38	5.90 Hyo Co 52.326 .5 1: 40.7 5.55 10.22	draulic Deponveyance: Right: 1 180.5 1 7 35. 6.3 2 11.4	th: 8.06 116403.6 246.915 183.5 3 33 8 6. 5 11.	9 0 1186.5 .9 63 60
X STA. A(I) V(I) D(I)	Tross-Section Bank Stat 1152.3)) 1186.5	0.000 Ven Area: ions -> I	elocity: 763.22 Left: 11 0 1176 45.8 4.91 8.38 1192 32.5	5.90 Hyc 52.326 .5 13 40.7 5.53 10.22	draulic Deponveyance: Right: 1 180.5 1 7 35. 8 6.3 2 11.4 194.8 1 4 31.	th: 8.06 116403.6 246.915 183.5 3 33 8 6. 5 11. 197.5	9 0 1186.5 .9 63 60 1200.2
X STA. A(I) V(I) D(I) X STA. A(I) V(I)	Cross-Section Bank Stat 1152.3)) 1186.5	0.000 Ven Area: ions -> I	elocity: 763.22 Left: 11 0 1176 45.8 4.91 8.38 3 1192 32.5 6.92	5.90 Hyc Cc 52.326 .5 1: 40.7 5.55 10.22 .1 1: 31.4 7.16	draulic Deponveyance: Right: 1 180.5 1 7 35. 8 6.3 2 11.4 194.8 1 4 31. 5 7.2	th: 8.06 116403.6 246.915 183.5 3 33 8 6. 5 11. 197.5 1 31 4 7.	9 0 1186.5 .9 63 60 1200.2 .1
X STA. A(I) V(I) D(I) X STA. A(I)	Cross-Section Bank Stat 1152.3)) 1186.5	0.000 Ven Area: ions -> I	elocity: 763.22 Left: 11 0 1176 45.8 4.91 8.38 3 1192 32.5 6.92	5.90 Hyc Cc 52.326 .5 1: 40.7 5.55 10.22 .1 1: 31.4 7.16	draulic Deponveyance: Right: 1 180.5 1 7 35. 8 6.3 2 11.4 194.8 1 4 31. 5 7.2	th: 8.06 116403.6 246.915 183.5 3 33 8 6. 5 11. 197.5	9 0 1186.5 .9 63 60 1200.2 .1
X STA. A(I) V(I) D(I) X STA. A(I) V(I) D(I)	Cross-Section Bank Stat 1152.3)) 1186.5	0.000 Ven Area: ions -> I	elocity: 763.22 Left: 11 0 1176 45.8 4.91 8.38 1192 32.5 6.92 11.60	5.90 Hyd Co 52.326 .5 1: 40.7 5.55 10.22 .1 1: 31.4 7.16	draulic Deponveyance: Right: 1 180.5 1 7 35. 8 6.3 2 11.4 194.8 1 4 31. 5 7.2 0 11.6	th: 8.06 116403.6 246.915 183.5 3 33 8 6. 5 11. 197.5 1 31 4 7. 0 11.	9 0 1186.5 .9 63 60 1200.2 .1 24
X STA. A(I) V(I) D(I) X STA. A(I) V(I) D(I) X STA.	Tross-Section Bank Stat 1152.3)) 1186.5	0.000 Ven Area: ions -> I	elocity: 763.22 Left: 11 1176 45.8 4.91 8.38 1192 32.5 6.92 11.60	5.90 Hyd 52.326 .5 1: 40.: 5.55 10.22 .1 1: 31.4 7.16 11.60	draulic Deponveyance: Right: 1 180.5 1 7 35. 8 6.3 2 11.4 194.8 1 4 31. 5 7.2 0 11.6	th: 8.06 116403.6 246.915 183.5 3 33 8 6. 5 11. 197.5 1 31 4 7. 0 11.	9 0 1186.5 .9 63 60 1200.2 .1 24 60
X STA. A(I) V(I) D(I) X STA. A(I) V(I) D(I) X STA. A(I)	Tross-Section Bank Stat 1152.3)) 1186.5) 1200.2	0.000 Ven Area: ions -> I	elocity: 763.22 deft: 11 1176 45.8 4.91 8.38 1192 32.5 6.92 11.60 1205 31.3	5.90 Hyd 52.326 .5 13 40.7 5.53 10.22 .1 13 .7.16 11.60 .6 12	draulic Deponveyance: Right: 1 180.5 1 7 35. 8 6.3 11.4 194.8 1 4 31. 7 .2 0 11.6	th: 8.06 116403.6 246.915 183.5 3 33 8 6.5 11. 197.5 1 31 4 7. 0 11. 211.1	9 0 1186.5 .9 63 60 1200.2 .1 24 60
X STA. A(I) V(I) D(I) X STA. A(I) V(I) D(I) X STA.	Cross-Section Bank Stat 1152.3)) 1186.5) 1200.2	0.000 Ven Area: ions -> I 1171.0 68.3 3.30 3.65 1189.3 32.9 6.83 11.60 1202.9 31.3 7.19	elocity: 763.22 Left: 11 1176 45.8 4.91 8.38 1192 32.5 6.92 11.60 1205 31.3 7.19	5.90 Hyd 52.326 .5 13 40.7 5.53 10.22 .1 13 7.16 11.60 .6 12 7.17	draulic Deponveyance: Right: 1 180.5 1 7 35. 8 6.3 2 11.4 194.8 1 4 31. 5 7.2 0 11.6	th: 8.06 116403.6 246.915 183.5 3 33 8 6.5 11. 197.5 1 31 4 7. 0 11. 211.1 1 33 2 6.	9 0 1186.5 .9 63 60 1200.2 .1 24 60
X STA. A(I) V(I) D(I) X STA. A(I) V(I) D(I) X STA. A(I) V(I) D(I) X STA.	Cross-Section Bank Stat 1152.3 1186.5 1200.2	0.000 Ven Area: ions -> I 1171.0 68.3 3.30 3.65 1189.3 32.9 6.83 11.60 1202.9 31.3 7.19 11.60	elocity: 763.22 Left: 11 1176 45.8 4.91 8.38 1192 32.5 6.92 11.60 1205 31.3 7.19 11.60	5.90 Hyc 52.326 .5 1: 40.7 5.55 10.22 .1 1: 31.4 7.16 .6 1: 31.5 7.15 11.60	draulic Deponveyance: Right: 1 180.5 1 7 35. 8 6.3 2 11.4 194.8 1 4 31. 5 7.2 11.6 208.3 1 7 32. 1 7.0 11.6	th: 8.06 116403.6 246.915 183.5 3 33 8 6.5 11. 197.5 1 31 4 7. 0 11. 211.1 1 33 2 6. 0 11.	9 0 1186.5 .9 63 60 1200.2 .1 24 60 1213.9 .0 82 60
X STA. A(I) V(I) D(I) X STA. A(I) V(I) D(I) X STA. A(I) V(I) D(I) X STA.	Cross-Section Bank Stat 1152.3 1186.5 1200.2	0.000 Ven Area: ions -> I 1171.0 68.3 3.30 3.65 1189.3 32.9 6.83 11.60 1202.9 31.3 7.19 11.60 1216.8 33.1	elocity: 763.22 deft: 11 1176 45.8 4.91 8.38 1192 32.5 6.92 11.60 1205 31.3 7.19 11.60	5.90 Hyd 52.326 .5 13 40.7 5.53 10.22 .1 13 31.6 7.16 11.60 .6 12 31.3 7.11 11.60	draulic Deponveyance: Right: 1 180.5 1 7 35. 8 6.3 2 11.4 194.8 1 4 31. 7 .2 0 11.6 208.3 1 7 32. 1 7.0 0 11.6	th: 8.06 116403.6 246.915 183.5 3 33 8 6.5 11. 197.5 1 31 4 7. 0 11. 211.1 1 33 2 6. 0 11.	9 0 1186.5 .9 63 60 1200.2 .1 24 60 1213.9 .0 82 60
X STA. A(I) V(I) D(I) X STA. A(I) V(I) D(I) X STA. A(I) V(I) D(I) X STA.	1152.3)) 1186.5) 1200.2	0.000 Ven Area: ions -> I 1171.0 68.3 3.30 3.65 1189.3 32.9 6.83 11.60 1202.9 31.3 7.19 11.60 1216.8 33.1 6.81	elocity: 763.22 deft: 11 1176 45.8 4.91 8.38 1192 32.5 6.92 11.60 1205 31.3 7.19 11.60 1219 35.5 6.34	5.90 Hyd 52.326 .5 13 40.7 5.53 10.22 .1 13 31.4 7.16 .6 12 .7 13 11.60 .8 12 39.3 5.73	draulic Deponveyance: Right: 1 180.5 1 7 35. 8 6.3 2 11.4 194.8 1 4 31. 5 7.2 11.6 208.3 1 7 32. 1 7.0 11.6	th: 8.06 116403.6 246.915 183.5 3 33 8 6.5 11. 197.5 1 31 4 7. 0 11. 211.1 1 33 2 6. 0 11. 228.8 3 67 7 3.	9 0 1186.5 .9 63 60 1200.2 .1 24 60 1213.9 .0 82 60 1246.9

```
******************* W S P R O ***************
       Federal Highway Administration - U. S. Geological Survey
              Model for Water-Surface Profile Computations.
             Input Units: English / Output Units: English
     *-----*
              I-74 RAMP OVER SPRING CREEK I74-4-4415DRA
         COUNTY: VERMILLION
                                    OUAD: PERRYSVILLE 93C
             7-30-97
                                        JOHN T. WILSON
         Beginning Velocity Distribution For Header Record BRDGE ***
         SRD Location: 126.000 Header Record Number 3
      Water Surface Elevation: 556.400
                                                   Element # 1
      Flow: 6600.000 Velocity: 6.86 Hydraulic Depth: 9.207
      Cross-Section Area: 962.33 Conveyance: 159975.40
         Bank Stations -> Left: 1147.209 Right: 1251.727
                   1168.3 1174.5 1178.9
                                                  1182.4
X STA.
          1147.2
                                                            1185.5
                   86.9 58.8 50.8
3.80 5.61 6.50
                                               45.5
7.26
  A(I)
                                                           42.4
                                                           7.78
  V(I)
                   4.12
                            9.46
                                     11.53
                                                13.07
                                                          13.60
 D(I)
                                                 1197.3
X STA. 1185.5 1188.5 1191.5 1194.4
                                                             1200.1

      41.2
      40.6
      39.3
      38.8
      38.8

      8.02
      8.12
      8.40
      8.50
      8.50

      13.60
      13.60
      13.60
      13.60
      13.60

 A(I)
 V( I )
 D(I)
X STA. 1200.1
                                        1208.8
                   1203.0
                              1205.9
                                                  1211.7
                                                             1214.7
                 39.1 39.1 39.5 39.2 41.9
8.45 8.45 8.35 8.41 7.87
13.60 13.60 13.60 13.60 13.60
 A(I)
 V( I )
 D(I)
X STA. 1214.7 1217.8 1221.1
                                       1225.4
                                                 1231.4
                                                            1251.7

      41.3
      44.8
      50.2
      58.0
      86.1

      8.00
      7.36
      6.58
      5.69
      3.83

 A(I)
 V( I )
                  13.60 13.31 11.83
 D(I)
                                                  9.70
    ****************** W S P R O **************
       Federal Highway Administration - U. S. Geological Survey
             Model for Water-Surface Profile Computations.
             Input Units: English / Output Units: English
              I-74 RAMP OVER SPRING CREEK I74-4-4415DRA
         COUNTY: VERMILLION QUAD: PERRYSVILLE 93C
             7-30-97
                                        JOHN T. WILSON
  *** Live-Bed Contraction Scour Calculations for Header Record BRDGE ***
                    Constants and Input Variables
            *----*
            Bed Material Transport Mode Factor (k1): .64
            Total Pier Width Value (Pw): 3.000
            *----*
```

```
-- Flow --
                        -- Width --
                                    --- X-Limits ---
   Depth Contract Approach Contract Approach Side Contract Approach
  -----
   -.694 4500.000 3523.816 91.000 59.000 Left: 1153.000 1206.000
  ..... Approach Channel Depth: 10.377 ..... Right: 1247.000 1265.000
* Negative Scour Depth Encountered - Check If Variables Are Reasonable *
2
   .078 6600.000 4730.451 91.000 59.000 Left: 1153.000 1206.000
  ..... Approach Channel Depth: 12.665 ..... Right: 1247.000 1265.000
  ******************* W S P R O ***************
     Federal Highway Administration - U. S. Geological Survey
          Model for Water-Surface Profile Computations.
          Input Units: English / Output Units: English
   *-----
          I-74 RAMP OVER SPRING CREEK I74-4-4415DRA4415DRA
                           OUAD: PERRYSVILLE 93C
       COUNTY: VERMILLION
          7-30-97
                                JOHN T. WILSON
      *** Pier Scour Calculations for Header Record BRDGE ***
                Constants and Input Variables
                  Pier Width: 1.500
          *----*
                                (K1): 1.00
           Pier Shape Factor
           Flow Angle of Attack Factor (K2): 2.00
           Bed Condition Factor
                               (K3): 1.10
           Bed Material Factor
Velocity Multiplier
                                (K4): 1.00
                               (VM): 1.00
           Depth Multiplier
                                (YM): 1.00
          Scour --- Localized Hydraulic Properties --- -- X-Stations --
               WSE Depth Velocity Froude # Left Right
   -----
                                   .375 1138.000 1264.000
1
   8.85 4500.000 554.351 11.551 7.236
   9.70 6600.000 556.376 13.576 8.526 .408 1138.000 1264.000
2
   ******************* W S P R O ***************
     Federal Highway Administration - U. S. Geological Survey
          Model for Water-Surface Profile Computations.
          Input Units: English / Output Units: English
   *----
          I-74 RAMP OVER SPRING CREEK I74-4-4415DRA
      COUNTY: VERMILLION
                           QUAD: PERRYSVILLE 93C
         7-30-97
                               JOHN T. WILSON
```

*** Pier Scour Calculations for Header Record BRDGE ***

Constants and Input Variables

Pier Width: 1.50	0	
*		*
Pier Shape Factor	(K1):	1.00
Flow Angle of Attack Factor	(K2):	2.00
Bed Condition Factor	(K3):	1.10
Bed Material Factor	(K4):	1.00
Velocity Multiplier	(VM):	1.00
Depth Multiplier	(YM):	1.00
*		*

	Scour	Localized Hydraulic			Properties		X-Stations	
#	Depth	${ t Flow}$	WSE	Depth	Velocity	Froude #	Left	Right
1	8.85	4500.000	554.351	11.551	7.236	.375	1138.000	1264.000
2	9.70	6600.000	556.376	13.576	8.526	.408	1138.000	1264.000

ER